

CO₂ CONVERSION ENHANCEMENT IN A PERIODICALLY OPERATED SABATIER REACTOR: NONLINEAR FREQUENCY RESPONSE ANALYSIS AND SIMULATION-BASED STUDY

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Introduction

Forced periodic operations

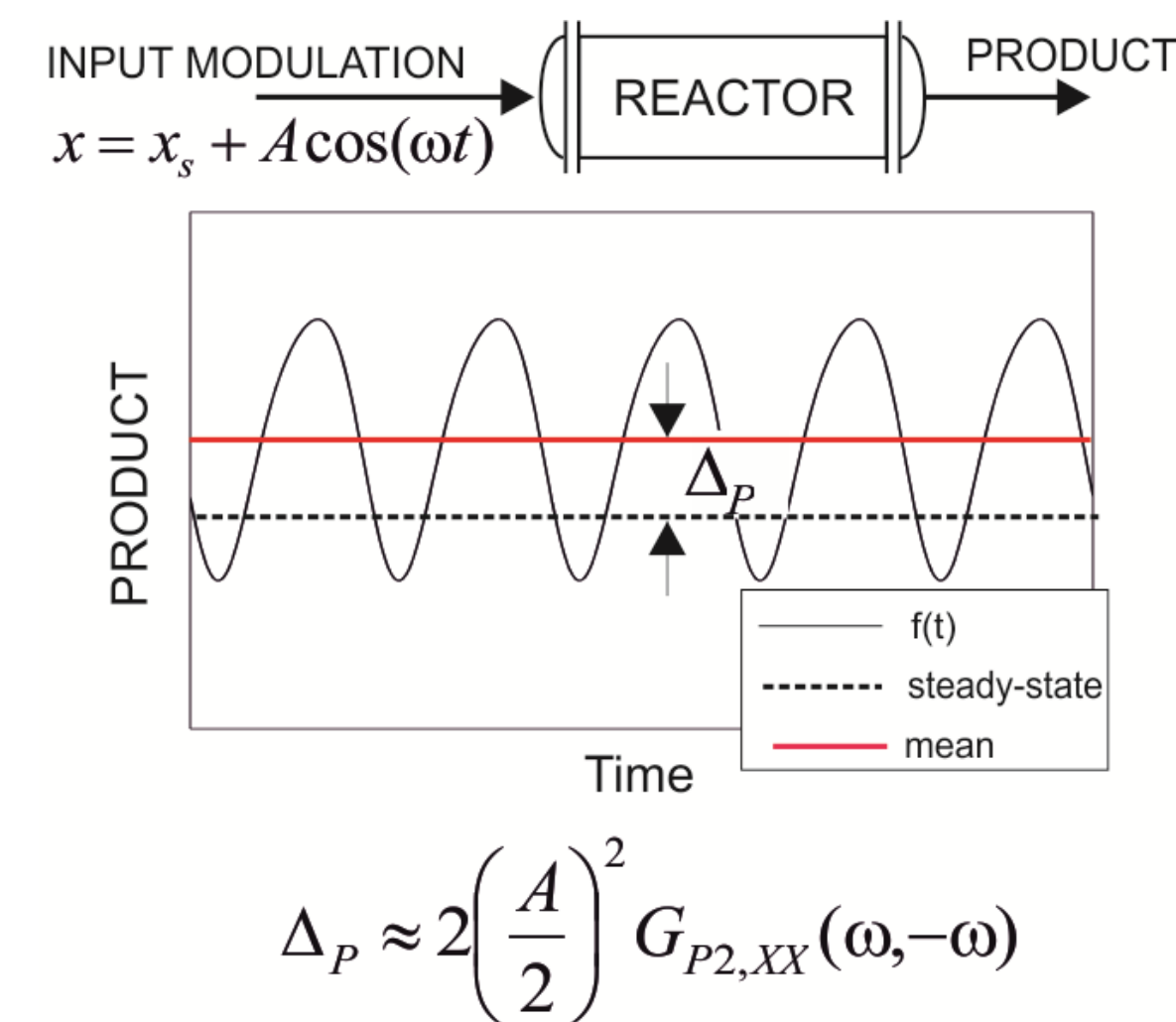
- One aspect of Process Intensification
- In some cases, the process performance can be enhanced by periodic modulation of some inputs around a chosen steady-state

Nonlinear Frequency Response Method

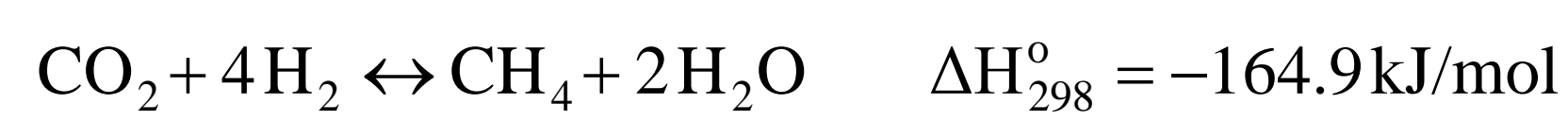
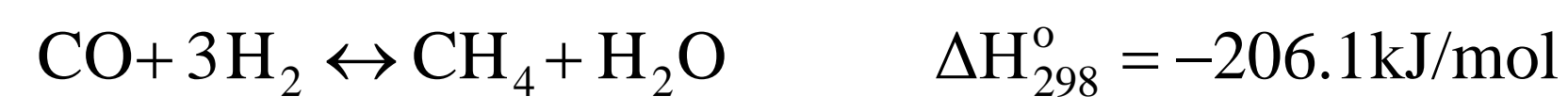
- Frequency response of a stable weakly nonlinear system is defined by a set of **Frequency Response Functions (FRFs)** of the first, second, third, ... order ($G_1(\omega)$, $G_2(\omega_1, \omega_2)$, $G_3(\omega_1, \omega_2, \omega_3), \dots$)
- The FR consists of indefinite number of harmonics and a **non-periodic term**

$$y = y_{DC} + B_I \cos(\omega t + \phi_I) + B_{II} \cos(2\omega t + \phi_{II}) + B_{III} \cos(3\omega t + \phi_{III}) + \dots$$

- y_{DC} – the non-periodic term – responsible for average performance of the periodic process – defines the process improvement through periodic operation ($\Delta \equiv y_{DC}$)
- **NFR method:** y_{DC} – non-periodic term proportional to $G_2(\omega, -\omega)$ – the asymmetrical second order (ASO) FRF
- Applicable to single and multiple input modulation
- Applicable to any shape of the periodic input



THIS WORK: Application to Sabatier reaction



Mathematical model:

- **Model assumptions:** CSTR, isothermal, diluted reaction system, constant total pressure
- **Model equations (dimensionless):**

$$\frac{du_i}{d\tau} = u_{if} - u_i + Da(\alpha_{i1}\kappa_1 f_1 + \alpha_{i2}\kappa_2 f_2 + \alpha_{i3}f_3)$$

$i = \text{CO}_2, \text{H}_2, \text{CH}_4, \text{CO}, \text{ and } \text{H}_2\text{O}$

$$u_i = \frac{c_i}{c_{if}} \quad \tau = \frac{t}{L/v_g} \quad Da = \frac{W_c k_3}{F_{if} \sqrt{P}}$$

$$\kappa_1 = \frac{k_1}{k_3} = \frac{A_1}{A_3} \exp\left(\frac{E_{a3} - E_{a1}}{R_g T}\right)$$

$$\kappa_2 = \frac{P^{1.5} k_2}{k_3} = \frac{P^{1.5} A_2}{A_3} \exp\left(\frac{E_{a3} - E_{a2}}{R_g T}\right)$$

CO₂ conversion in periodic conditions

$$X_{av, \text{CO}_2} = \frac{u_{\text{CO}_2, f} F_{if, ss} - (u_{\text{CO}_2} F_{if})^m}{u_{\text{CO}_2, f} F_{if, ss}}$$

Kinetic model

(adapted from J. Xu, G. F. Froment, *AIChE J.* 1989, 35, 88-96.)

$$f_1 = \frac{1}{\sqrt{\delta}} \frac{u_{\text{CH}_4} u_{\text{H}_2\text{O}}}{u_{\text{H}_2}^{2.5}} - \delta^{1.5} \frac{u_{\text{H}_2}^{0.5} u_{\text{CO}}}{k_{1,eq}}$$

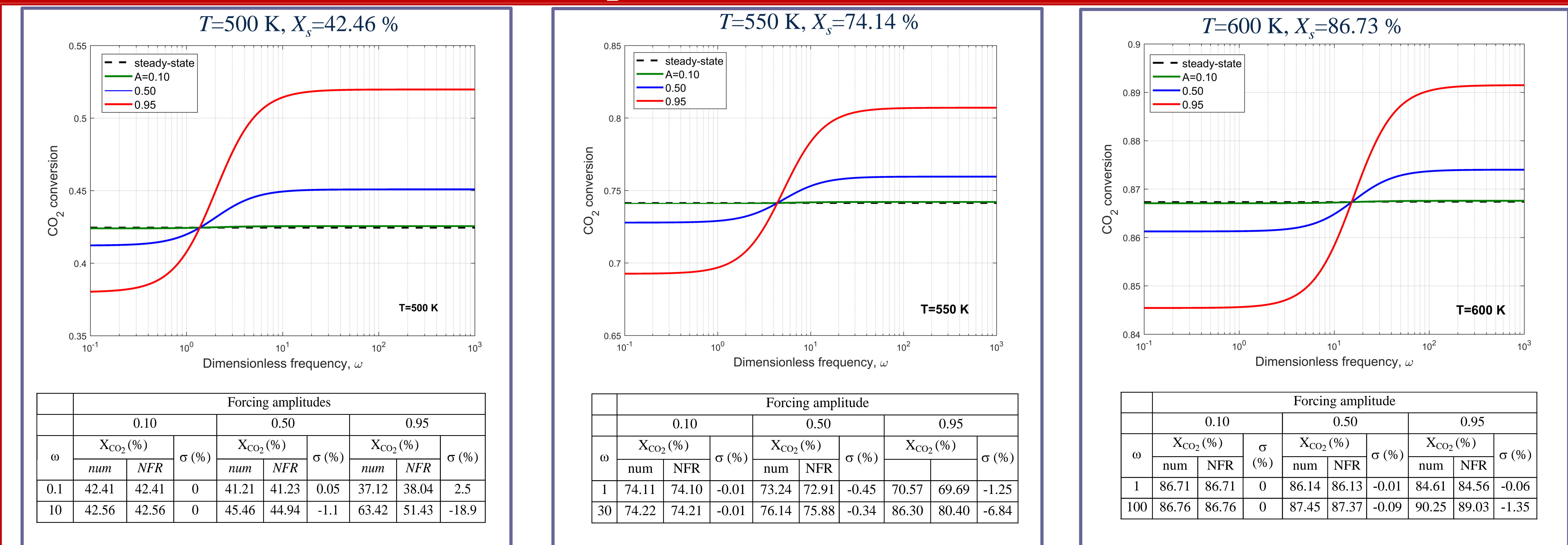
$$f_2 = \delta \left(\frac{u_{\text{CO}} u_{\text{H}_2\text{O}}}{u_{\text{H}_2}} - \frac{u_{\text{CO}_2}}{k_{2,eq}} \right)$$

$$f_3 = \frac{1}{\sqrt{\delta}} \frac{u_{\text{CH}_4} u_{\text{H}_2\text{O}}^2}{u_{\text{H}_2}^{3.5}} - \delta^{1.5} \frac{u_{\text{H}_2}^{0.5} u_{\text{CO}_2}}{k_{3,eq}}$$

$$k_{j,eq} = \frac{K_{j,eq}}{P^2} \quad j = 1, 3; \quad k_{2,eq} = K_{2,eq}$$

Model parameters from in-house Measurements (Uni. Waterloo)

RESULTS – CO₂ conversion for flow-rate modulation



Some numerical examples

