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Characterization of sodium alginate/D-limonene emulsions and respective calcium alginate/D-limonene beads produced by electrostatic extrusion

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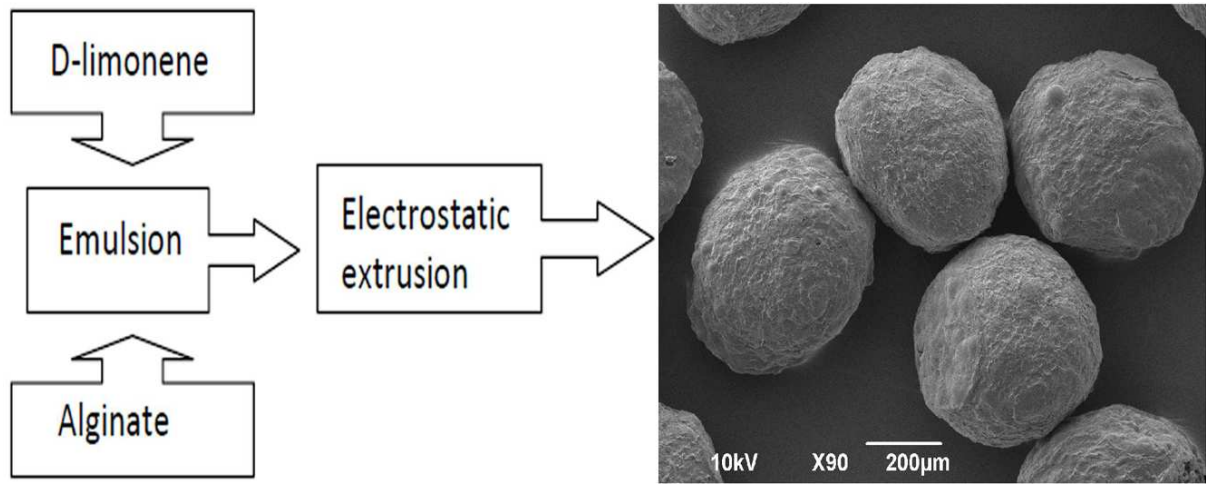
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1           **Characterization of sodium alginate/D-limonene emulsions and respective calcium**  
2           **alginate/D-limonene beads produced by electrostatic extrusion**

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16  
17           **Abstract**

18  
19           In this study, calcium alginate beads immobilizing D-limonene (solid systems) have been  
20           manufactured starting from emulsions of this flavor in sodium alginate (liquid systems). The  
21           effects of alginate concentration (0.02 and 0.03 g/mL) and flavor content (5 and 10 %w/w) on  
22           viscosity, conductivity and stability of emulsions were investigated. The flavor droplets in  
23           emulsions are bigger as polymer solution is more concentrated and contains more of the flavour.  
24           When emulsions have been subjected to electrostatic extrusion and upon Na<sup>+</sup>-Ca<sup>2+</sup> ion exchange,  
25           smaller (~960 to ~1450 μm) and less spherical beads were obtained (sphericity factor 0.003 to

26 0.21) compared to beads produced by simple dripping technique (without electrostatic field).  
27 When wet beads were air dried, they shrunk less if they had higher content of the flavour. Novel  
28 mathematical model describing swelling kinetics of dried beads is developed. In this work, D-  
29 limonene was efficiently immobilized within Ca-alginate beads (immobilization efficiency ~50  
30 to ~77%) and its thermal stability was confirmed by TG/MS analysis.

31

32 **Keywords:** immobilization; alginate; electrostatic extrusion; D-limonene; swelling.

33

## 34 1. Introduction

35

36 D-limonene is the major flavour compound of citrus oil and it has been widely used as a food  
37 flavor (Burdock, 2004; Sahraoui, Abert Vian, El Maataoui, Boutekedjiret, & Chemat, 2011) and  
38 medicament for tumor treatment (Nakaizumi, Baba, Uehara, Iishi, & Tatsuta, 1997; Uedo et al.,  
39 1999; Del Toro-Arreola et al., 2005). Nevertheless, it has highly lipophilic nature which results  
40 in poor absorption and palatability. Besides, limonene is susceptible to oxidative degradation and  
41 this results in the loss of lemon-like flavour under normal storage condition (Soottitantawat,  
42 Yoshii, Furuta, Ohkawara, & Linko, 2003). Aroma such is limonene can be encapsulated in  
43 order to improve its functionality and stability in products. Apart from protection at ambient  
44 conditions (air humidity, oxygen, etc.), encapsulation should provide thermal protection during  
45 food processing. Another possible benefit of aroma's encapsulation is superior ease of handling,  
46 as conversion of liquid aroma oil into a powder is achieved. Various encapsulation methods have  
47 been previously proposed for encapsulation of liquid aromas such as limonene. Among them,  
48 spray-drying is the most popular method of producing flavor powders (Soottitantawat et al.,

49 2005; Zuidam & Heinrich, 2010). However, it is rather difficult to remove water by vaporization  
50 while retaining the flavours that are much more volatile than water (Soottitantawat et al., 2003),  
51 and a lot of effort has to be invested in preventing flavor losses during spray-drying. Instead,  
52 extrusion/dropping techniques provide simple and safe processing for production of  
53 microspheres as biopolymer gel microbeads embedding oil droplets. Moreover, extrusion  
54 techniques have advantage when bigger particles (100-1000  $\mu\text{m}$  in contrast to small size 10-150  
55  $\mu\text{m}$  spray-dried aroma powders) are needed in order to create special visible or textural effects  
56 (for example in crunchy food products). Among extrusion techniques, electrostatic extrusion is  
57 the one suitable for processing polymer solutions in the wide range of viscosities and production  
58 of particles of desired and uniform size (Prüsse et al., 2008). It is based on the use of electrostatic  
59 forces to disrupt the liquid filament at the tip of a needle and to create a charged stream of small  
60 droplets. The excessive investigations were performed to determine the specific influence of  
61 each of the processing parameters on the diameter of microbeads (Bugarski et al., 2006). In this  
62 study, calcium alginate gel was employed as the matrix for D-limonene immobilization, as it has  
63 been determined that calcium-alginate does not adversely affect the release of the flavour during  
64 consumption (De Roos, 2003; 2006). Also, alginate gel beads are suitable for application in food  
65 products as they showed good properties during gastro-intestinal evaluations (Rayment et al.,  
66 2009). One of the critical points of the encapsulation of lipophilic flavours is low stability of  
67 alginate-flavour emulsions. In order to conquer the instability induced by the high hydrophilicity  
68 of alginate particles several strategies have been proposed, such as addition of conventional  
69 surfactants (You, Rafat, & Auguste, 2011) and coating with chitosan to modify the  
70 hydrophilicity of alginate particles (Nan et al, 2014). However, the addition of any of this  
71 compounds inevitable increases costs, furthermore, the usage of surfactants is limited in food

72 applications and it unavoidably results in low biocompatibility of alginate particles. Therefore, in  
73 this work we tried to immobilize a flavour compound in alginate microspheres by internal  
74 gelation in the absence of surfactants, so that the flavor is only roughly stabilized by developed  
75 viscosity of alginate in aqueous systems.

76 The objective of the present study is to investigate the characteristics of alginate as a matrix  
77 material for immobilization of the liquid flavor such as D-limonene. We intend to reveal the  
78 interdependence of characteristics (such as viscosity, conductivity, stability and flavor droplet  
79 size distribution) of Na-alginate/D-limonene emulsions (liquid systems) with the properties of  
80 the corresponding Ca-alginate/D-limonene beads (solid systems) produced by electrostatic  
81 extrusion technique. Thus, the effects of immobilization process on the flavour's physical and  
82 thermal stabilities were examined. For assessment of the thermal stability, the immobilized  
83 flavor is tested by thermogravimetric/mass spectrometry analysis. Beside hydrogel beads, dried  
84 forms of those were also investigated as they are stronger than non-dried hydrogel beads and  
85 more convenient for long shelf life products. Rehydration of air-dried beads was examined in  
86 detail, as controlled rehydratability is important to many food applications (e.g. preparations of  
87 instant products).

## 88 89 **2. Materials and methods**

### 90 91 *2.1. Chemicals*

92 D-limonene was obtained from HiMedia Laboratories Pvt.Ltd (Mumbai, India). Sodium  
93 alginate (from *Macrocystis pyrifera*, molecular weight: 80000-120000. M/G ratio: 1.56) was  
94 purchased from Sigma (St. Louis, USA). Calcium chloride dihydrate was purchased from Acros  
95 Organics (New Jersey, USA), while n-hexane (HPLC grade) was supplied from Carlo Erba

96 Reagenti SpA (Rodano, Italy). All other chemicals were of analytical reagent grade and they  
97 were used without any further purification.

98

## 99 *2.2. Preparation and characterization of the liquid systems*

100 The preparation of liquid systems was the first step of immobilization process. The liquid  
101 systems used in this study were water solutions of Na-alginate (concentration of 0.02 g/mL or  
102 0.03 g/mL) and Na-alginate/D-limonene emulsions (5% w/w or 10% w/w of dispersed D-  
103 limonene in 0.02 g/mL or 0.03 g/mL Na-alginate). The compositions of the liquid systems which  
104 are denoted as  $S_a^b$  (where  $a$  is the concentration of Na-alginate (in g/mL) while  $b$  is D-limonene  
105 concentration in %w/w) and used in this study are summarized in Table 1.

106

### 107 **Table 1**

108

## 109 *2.3. Preparation of D-limonene/Na-alginate emulsions*

110 D-limonene was added into the Na- alginate solutions under vigorous mixing at 10.000 rpm  
111 for 5 minutes using mechanical stirrer Ultra-Turrax® T25 (Janke and Kunkel Ika-Labortechnik,  
112 Staufen, Germany).

## 113 *2.4. Measurements of rheological features of liquid systems*

114 Viscosity measurements (in triplicate) were carried out using a viscometer (Rheotest 2,  
115 MLW, OT Medingen, Ottendorf-Okrilla, Germany,) in the range of the shear rate from 0 to  
116  $1300\text{s}^{-1}$  during 7 min. The cylinder measuring configuration was S/S1 which has the viscosity  
117 range between 20 and  $10^5$  mPa·s. The experimental results were fitted with Power law model:

$$118 \quad \tau = k \times \dot{\gamma}^n \quad (1)$$

119 and consistency ( $k$ ), and flow index ( $n$ ) were determined. In power law equation,  $\tau$  is the shear  
120 stress and  $\dot{\gamma}$  is the shear rate.

121 The thixotropic properties of the liquid samples were characterized by using hysteresis  
122 experiments which consisted of a three step operation (upward curve, plateau curve and  
123 downward curve): an increasing shear rate ramp at a constant shear rate of  $3.10 \text{ s}^{-1}$  from 0 to  
124  $1300 \text{ s}^{-1}$ , followed by a plateau at the maximum shear rate for 50 s, and thereafter, the ramp was  
125 reversed (with the same rate) to measure downward flow curve from 1300 to  $0 \text{ s}^{-1}$ . For time-  
126 dependent samples, the area enclosed between up curves and down curves obtained by increasing  
127 and decreasing shear rate measurements was calculated as the difference between integrating the  
128 area for forward and backward measurements from  $\dot{\gamma}_1$  (initial shear rate) to  $\dot{\gamma}_2$  (final shear rate):

$$129 \quad \text{Hysteresis loop area} = \int_{\dot{\gamma}_1}^{\dot{\gamma}_2} k \dot{\gamma}^n - \int_{\dot{\gamma}_1}^{\dot{\gamma}_2} k' \dot{\gamma}^{n'} \quad (2)$$

130 Where  $k$ ,  $k'$ , and  $n$ ,  $n'$  are the consistency coefficient and flow index behavior for forward and  
131 backward measurements, respectively.

### 132 2.5. Conductivity of the liquid systems

133 The conductivities of the solutions and the emulsions were measured (in triplicate) using  
134 conductometer InoLab<sup>®</sup> 720 (WTW GmbH, Weilheim, Germany), at room temperature.

### 135 2.6. Stability of the emulsions

136 Stability of the emulsions was tested by applying the procedure reported by Chan (2011a).  
137 Briefly,  $\sim 50 \text{ mL}$  of an alginate-flavour emulsion was left to stand for 1 hour in order to  
138 investigate emulsion stability. The volume of phases which had been formed during the period of



139 1 hour was measured (in triplicate). Emulsion stability was calculated as a quotient of the volume  
140 of the remaining emulsion and volume of the initial emulsion and expressed in %.

#### 141 *2.7. D-limonene droplet size measurements*

142 The flavor droplet size of the each of D-limonene/Na-alginate emulsion formulations was  
143 determined as a numeric average of 100 droplets which diameters were measured under an  
144 optical microscope (Olympus CX41RF, Tokyo, Japan) equipped with a camera (Olympus U-  
145 CMAD3, Tokyo, Japan) and coupled with the image analysis program “Cell<sup>A</sup>” (Olympus,  
146 Tokyo, Japan).

#### 147 *2.8. Preparation and characterization of the solid systems*

148 The solid systems were produced by the procedure developed previously by Nedović et al.  
149 (2001) and Levic et al. (2013). The schematic presentation of the immobilization process is  
150 shown in Fig. 1a. Electrostatic immobilization unit (VAR V1, Nisco Engineering Inc., Zurich,  
151 Switzerland) used in this work is a compact system equipped with a high voltage unit, magnetic  
152 stirrer and protective cage. Spherical droplets were formed by extrusion of the liquid systems  
153 through a blunt stainless steel needle using a syringe pump (Pump 11, Harvard Apparatus,  
154 Holliston, US). The needle was grounded, while the collecting solution (CaCl<sub>2</sub> in water solution  
155 with a concentration of 0.015 g/mL) was positively charged. All samples (Table 1) were  
156 extruded simply by dripping without applying any voltage (formulations no. 1 to 6), and the  
157 samples with the same compositions were extruded in the electrostatic field maintained with a  
158 constant voltage of 6.5kV (formulations no. 7 to 12). Formations of liquid drops during extrusion  
159 are shown in Fig. 1b (Fig. 1b<sub>1</sub>-formation of liquid drops without electrostatic force; Fig. 1b<sub>2</sub>-  
160 formation of liquid drops by electrostatic force). The distance between the needle tip (22 gauges)  
161 and the collecting solution was 2.5 cm, while the flow rate of the liquid systems was 70 ml/h.

162 After formation of the beads, they were left in hardening solution without stirring for 60 min in  
163 order to assure finishing of the gelling process. The formed alginate beads were removed from  
164 the CaCl<sub>2</sub> solution by filtration and washed with distilled water. In this way hydrogel beads  
165 were obtained. In order to produce dried forms of beads, hydrogel beads were air-dried at 25 °C  
166 for 48h.

167

168 **Fig. 1.**

169

### 170 2.9. Analysis of the beads dimensions and shape

171 Dimensions and shape of hydrogel and dried beads were evaluated by binocular microscope  
172 Leica XTL-3 400D (Leica, Wetzlar, Germany), equipped with a camera (DC 300, Leica,  
173 Wetzlar, Germany) and software for measuring (IM 1000, Leica, Wetzlar, Germany). For each  
174 formulation, a numeric average of average diameters of 100 beads was taken as a mean diameter,  
175 whereas the diameter for each bead was calculated as an average of the largest dimension ( $d_{max}$ )  
176 and the smallest dimension ( $d_{min}$ ) perpendicular to the largest diameter of the microbead.

177 The deformation of the beads from regular spherical shape was calculated and represented as  
178 Sphericity factor (SF). Sphericity factor was calculated as described by Chan, Lee, Ravindra, &  
179 Poncelet (2009). Briefly, the beads diameters were measured as described above and Sphericity  
180 factor was calculated by using Equation (3):

181

$$182 \text{ Sphericity factor}(SF) = \frac{d_{max} - d_{min}}{d_{max} + d_{min}} \quad (3)$$

183

184 where  $d_{max}$  is the maximum diameter and  $d_{min}$  is the minimum diameter of the beads  
185 perpendicular to  $d_{max}$ .

186 The reduction in the beads size after drying was expressed by Shrinkage factor ( $k_{SF(drying)}$ ) and  
187 calculated according the Equation (4) (Chan et al., 2011b):

188  
189 
$$k_{SF(drying)} = (d_b - d_{b(dry\ beads)}) / d_b \quad (4)$$
  
190

191 where  $d_b$  was the diameter of the wet beads and  $d_{b(dry\ beads)}$  was the diameter of the beads after  
192 drying.

### 193 2.10. Scanning electron microscopy (SEM)

194 The microstructure of samples has been carried out by JEOL JSM-6390LV scanning electron  
195 microscope. Prior to the analysis the samples were covered with Au using a sputter coater Baltec  
196 scd 005 accessory.

### 197 2.11. D-limonene content determination

198 Half a gram of the dried beads was dissolved in 40 ml of sodium citrate (0.015 g/ml) in glass  
199 bottles and 5 ml of hexane was added. The flavor was extracted with hexane by heating the  
200 samples in glass bottles at 45 °C in a water bath for 15 min with intermittent mixing. The  
201 samples were then cooled down to room temperature and hexane was separated from the aqueous  
202 phase by centrifugation at 4000 rpm for 20 min. The content of D-limonene in the samples was  
203 determined by gas-chromatography and calculated from the standard calibration curve.  
204 Quantitative analysis was conducted using an Agilent 4890D gas chromatograph fitted with a  
205 HP-5MS 30m×0.25mm capillary column, with hydrogen as the carrier gas (constant flow rate of  
206  $1\text{ cm}^3\text{ min}^{-1}$ ) and flame-ionization detector (FID). The temperature program was: 40 °C for 9 min;  
207 then  $15\text{ °Cmin}^{-1}$  to 150 °C and held for 2 min. The temperatures of the injector and the detector  
208 were maintained during the analysis at 250 and 300°C, respectively. The calibration curve was

209 obtained using seven standard D-limonene solutions which were analyzed under the same  
210 conditions as the samples. Data acquisition was performed by GC Chem Station software.

211 Immobilization efficiency (E) was calculated on the basis of Equation (5):

$$212 \quad E = m_e / m_i \times 100\% \quad (5)$$

214 where  $m_e$  is the mass of encapsulated D-limonene and  $m_i$  is the initial mass of the flavor.

215 All samples were analyzed in duplicate and the data were presented as average values  $\pm$   
216 standard deviation values (SD).

217

### 218 *2.12. The study of beads swelling*

219 Swelling studies of the dried Ca-alginate beads (with and without the flavour) were carried out in  
220 two different swelling solutions: (1) distilled water and (2) phosphate buffer (10 mM, pH 7.4).

221 The weighed amount of the dried beads was immersed in 20 mL of the swelling solution at room  
222 temperature under shaking at 100 rpm. At previously defined time intervals, the beads were  
223 separated from the swelling solution, gently wiped with filter paper and weighed. The swelling  
224 ratio ( $M_t$ ) of the beads was calculated according to the Equation (6):

$$225 \quad M(t) = (w_1 - w_2) / w_2 \quad (6)$$

227 where  $w_1$  was the weight of the beads in the swollen state and  $w_2$  was the initial weight of the  
228 dried beads.

### 230 *2.13. Thermal analysis of the dried beads*

231 Thermal analysis of samples was carried out in a Setaram's TG/DSC111 apparatus coupled  
232 with mass spectrometer (Thermostar from Pfeifer, system equipped with a capillary connection).

233 The measurements were realized employing the simultaneous thermogravimetry/mass

234 spectrometry (TG/MS) technique under dynamic helium of a flow rate of 30 ml/min (pressure 1  
235 atm) using a heating rate of 5 °C/min. The targeted mass spectra (i.e. water, D-limonene) were  
236 selected according to data from the Spectral Database for Organic Compounds, AIST (SDBS).

#### 237 *2.14. Data analysis*

238 D-limonene droplet size as well as beads dimension were analyzed using the statistical  
239 package PSS 17.0 (SPSS Inc., Chicago, IL, USA). The obtained results were subjected to one-  
240 way analysis of variances (ANOVA) in order to determine the differences between multiple  
241 means in continuous variables. Statistical significance was set at  $p < 0.001$ . The means are  
242 further analyzed with Tukey's HSD test, to find those that differ. Eta-squared ( $\eta^2$ ) was a measure  
243 of effect size, ranging from 0 and 1.

244

### 245 **3. Results and discussion**

#### 246 *3.1. Characteristics of the liquid systems*

247 The properties of the liquid samples (Table 2) were examined as they play important roles in  
248 droplet formation upon processing of liquids by extrusion-dripping technique under electrostatic  
249 field.

250

#### 251 **Fig. 2.**

252

253 Viscosities of all liquid samples (liquid formulations presented in Table 1) were determined  
254 in the range of shear rate from 0 to 1300 s<sup>-1</sup>. As shown in Fig. 2, the viscosity decreased with the

255 increasing of shear rate for all liquid systems indicating shear thinning behavior. It can be  
256 inferred that this behavior of alginate probably originate from conformational changes and  
257 orientation of rigid polysaccharide alginate chains in the flow field, what is in accordance with  
258 the published data (Lee, Bouhadir, & Mooney, 2002), which demonstrate that alginate's rigid  
259 chain conformation affects mechanical properties of this polysaccharide. Shear viscosity of Na-  
260 alginate solutions and Na-alginate D/limonene emulsions increased with increasing the alginate  
261 concentration. This is a result of more intensive chain-chain interactions existing in the more  
262 concentrated solutions that express more pronounced non-Newtonian behavior (Manojlović,  
263 Đonlagić, Obradović, Nedović, & Bugarski, 2006). The parameters of the Power law model are  
264 presented in Table 2. The flow index ( $n$ ) varies from 0.51 to 0.63, which confirms the shear  
265 thinning behavior. Moreover, an increase in the sodium alginate concentration (from 2 to 3%  
266 w/v) at the same concentration of aroma confirmed an increase in the shear thinning which  
267 showed a decrease in the flow behavior index ( $n$ ). The consistency coefficient ( $k$ ) increased with  
268 the concentration of sodium alginate, which is in accordance to literature (Ma et al, 2014;  
269 Oliveira et al, 2010). At the same time, higher concentration of the flavour within Na-alginate  
270 caused slightly higher values of the viscosity; consequently,  $k$  values become higher with  
271 increasing the flavor content. The dispersed flavour probably acts as an additional barrier for  
272 conformational changes and orientation of rigid polysaccharide chains in flow field. This is in  
273 accordance with data reported in the study of Sosa-Herrera, Lozano-Esquivel, Ponce de León-  
274 Ramírez, & Martínez-Padilla (2012) where it was shown that dispersed oil particles also induced  
275 increase in viscosity of Na-alginate aqueous mixtures. As regarding the thixotropic properties,  
276 the upward and downward flow curves superpose for all the samples with the exception of  $S_{0.03}^{10}$ ,  
277 for which a small hysteresis loop was observed (see Fig.2). According to Ma, Lin, Chen, Zhao,

278 & Zhang (2014) and Tabeei, Samimi, Khorram & Moghadam (2012) sodium aqueous solutions  
279 in general exhibit a certain thixotropic property, and the greater the sodium alginate  
280 concentrations, the stronger the thixotropic properties. However, this was not observed by some  
281 authors, e.g. Oliveira et al. (2010) who claimed that alginate solutions even at high  
282 concentrations (up to 10 w/v %) did not present thixotropy. The hysteresis loop area for  $S_{0.03}^{10}$  was  
283 calculated according to eq. 2, with the consistency coefficient  $k$  and flow index  $n$  presented in  
284 Table 2 and consistency coefficient  $k'$  of  $10.40 \pm 1.01 \text{ Pa} \cdot \text{s}^{-0.51}$ , and flow index  $n'$  of  $0.51 \pm 0.01$   
285 (both obtained by fitting the downward flow curve with Power law model (eq.1)). Thus obtained  
286 value was  $12850 \text{ Pa s}^{-1}$ .

287 Conductivities of all liquid samples were measured, in order to examine the effects of  
288 particles' forming under electrostatic field. From the literature it is known that, by increasing  
289 conductivity of the polymer solution (for example by adding a small amount of an organic salt) it  
290 is possible to dramatically decrease the size of particles produced by electrohydrodynamic  
291 atomization (Xie, Lim, Phua, Hua, & Wang, 2006), the process based on the same principles as  
292 the one used here. However, the influence of conductivity has not been explored yet on the  
293 particular set-up of electrostatic extrusion. The results of conductivity measurements done here  
294 are presented in Table 2. Sodium alginate is a polyelectrolyte having high conductivity and the  
295 values obtained for pure Na-alginate (samples  $S_{0.02}^0$  and  $S_{0.03}^0$ ) are very close to literature data (Li  
296 et al., 2013). As expected, lower concentrated Na-alginate solutions appeared to be less able to  
297 conduct electricity. The results presented in this study indicate that D-limonene induce dumping  
298 effects and decrease in conductivity in the liquid systems (Table 2). The conductivity of  
299 solutions of sodium alginate is reduced by ~14% after adding the flavour, indicating that the  
300 flavour reduced the repulsive forces among the polyanionic sodium alginate molecules.

301 The stability of all prepared emulsions was estimated 1 h after they were left standing, as  
302 within this time interval it was possible to complete the immobilization process, including the  
303 formation of solid beads. In line with literature reports, emulsion stability is an important  
304 property from the viewpoint of the encapsulation efficiency as well as the product quality (Chan,  
305 2011a). It could be expected that concentration higher than 10 % w/w of the flavour would cause  
306 destabilization of the emulsion. However, our observation (screening for phase separation), as  
307 well as the analysis (Table 2) showed that emulsions with both concentrations of D-limonene  
308 (5% w/w and 10% w/w) were stable for a period of one hour. For the sake of comparison, Chan  
309 (2011a) has shown that emulsions of palm oil in alginate were stable for 1h if the alginate  
310 concentration was higher than 25 g/L. Furthermore, our measurements confirmed that stability  
311 did not depend appreciably on the amount of the dispersed phase (Table 2).

312

### 313 **Table 2**

314

315 The influence of concentrations of both components on the size of D-limonene droplets  
316 (obtained by light microscopy) is presented in Fig. 3. The size of droplets was measured in four  
317 different solutions: 5% w/w flavor in 0.02 g/mL Na-alginate ( $S_{0.02}^5$ ), 10% w/w flavor in 0.02  
318 g/mL Na-alginate ( $S_{0.02}^{10}$ ), 5% w/w flavour in 0.03 g/mL Na-alginate ( $S_{0.03}^5$ ), and 10% w/w flavor  
319 in 0.03 g/mL Na-alginate ( $S_{0.03}^{10}$ ). The size of D-limonene droplets within the solutions ranged  
320 from 1.0  $\mu\text{m}$  to 14.5  $\mu\text{m}$  for  $S_{0.02}^5$  from 1.5  $\mu\text{m}$  to 24.9  $\mu\text{m}$  for  $S_{0.02}^{10}$ , from 1.6  $\mu\text{m}$  to 38.5  $\mu\text{m}$  for  
321  $S_{0.03}^5$  and from 1.9  $\mu\text{m}$  to 52.1  $\mu\text{m}$  for  $S_{0.03}^{10}$ . The mean values for droplets size ranged from 4.9  
322  $\mu\text{m}$  for  $S_{0.02}^5$  to 11.7  $\mu\text{m}$  for  $S_{0.03}^{10}$ . The data were further analyzed with one-way ANOVA, which  
323 showed that the mean differences between droplets size in four different solutions were



324 statistically significant ( $F(3,384)=16.680$ ,  $p<0.001$ ). The means are further analyzed with  
325 Tukey's HSD test, to find those that differ. Post hoc comparisons using the Tukey HSD test  
326 indicated that the mean score for the droplets sizes in  $S_{0.03}^{10}$  was significantly different than the  
327 mean of the droplets sizes in other three samples. The droplets size in  $S_{0.03}^5$ , however, was  
328 significantly different than the droplets size in  $S_{0.03}^{10}$  only.

329 The results indicate that higher concentration of alginate influenced the appearance of D-  
330 limonene droplets with higher mean droplet sizes. This is expected, as hydrophilic  
331 polysaccharide hydrocolloid, such is alginate, should have a low surface activity. However, the  
332 opposite outcome is reported by Chan (2011a) who demonstrated that smaller oil droplets are  
333 developed if alginate is more concentrated. It seems that an increase in viscosity of the  
334 continuous phase elevates resistance for effective dispersion of flavour droplets. In order to get  
335 smaller flavour droplets and consequently, to create more stable emulsions, higher power inputs  
336 are needed and can be achieved, for example, by ultra high-pressure homogenization (Kaushik &  
337 Roos, 2007).

338

339 **Fig. 3.**

340

341 *3.2. Effects of the liquid systems structural organization and applied voltage on the beads*  
342 *properties*

343 The average size of the wet and dried beads is shown in box-plots (Fig. 4).

344

345 **Fig. 4.**

346

347 Without applying electrostatic field, wet beads with diameters in the range from ~2100 to  
348 ~2350  $\mu\text{m}$  were produced. Under the applied voltage of 6.5 kV (other processing parameters  
349 were the same) smaller beads were formed with diameters in the range from ~960 to ~1450  $\mu\text{m}$ .  
350 The mean differences between systems were tested with ANOVA, which showed that groups of  
351 data corresponding to different systems were significantly different ( $F(11,839)=75.739$ ,  
352  $p<0.001$ ). Tukey's post-hoc test showed significant difference between diameters of beads  
353 produced with and without electrostatic force.

354 From the results presented so far it follows that the increase in alginate concentration leads to  
355 statistically significant increase in hydrogel beads diameter in case of those produced by  
356 electrostatic extrusion ( $F(1,482)=8.009$ ,  $p=0.005$  for wet particles,  $F(1,367)=6.129$ ,  $p=0.014$  for  
357 dried particles). These findings can be comprehended as a consequence of increased viscosity of  
358 more concentrated Na-alginate solutions/emulsions, determined here and also elsewhere  
359 (Manojlović et al., 2006); while obviously, conductivity did not correlate with the size of beads.  
360 Also, it seems that the increase in viscosity deteriorated the beads uniformity. The observed  
361 increase in standard deviations is in agreement with mechanisms of droplet formation under  
362 action of the electrostatic field (Bugarski et al., 2006). Namely, a detachment of the main drop of  
363 the high-viscous solution at the tip of the needle is accompanied by detachment of the linking  
364 filament, which then brakes up into a large number of smaller droplets resulting in non-uniform  
365 size distribution. Since the size of dry particles has a direct relationship with the size of wet  
366 beads, the results for the size of dry beads seem to be qualitatively consistent with the correlation  
367 laws established for hydrogel forms. Fig.5A and 5B show microphotographs of the wet and dried  
368 beads produced by simple dripping technique (without applying electrostatic force) and  
369 electrostatic extrusion (by applying electrostatic force), respectively.

370

371 **Fig. 5.**

372

373 Since systems differ in amount of D-limonene, the influence of this factor was also observed  
374 and tested. ANOVA test showed that there is a statistically significant difference between  
375 diameters of beads with different content of D-limonene, both among wet beads  
376 ( $F(2,480)=3.912$ ,  $p=0.021$ ) and dried beads ( $F(2, 356)=51.033$ ,  $p<0.001$ ). Eta-squared ( $\eta^2$ )  
377 measure of the flavour concentration effect on beads size was 0.02 for wet beads, which is  
378 usually taken as small, and 0.22 for dried beads, which is taken as a large effect.

379 Sphericity factor (SF) was used to quantitatively express the roundness of the beads: the zero  
380 value designates a perfect sphere, while as higher the SF value is, more pronounced distortion of  
381 shape occurs. Sphericity factor for wet and dried beads formed under electrostatic field and for  
382 those formed by simple dropping under gravity (without electrostatic field) are shown in Table 3.  
383 The results show that elongated forms of hydrogel beads were produced when processing  
384 flavour in 0.03 g/mL alginate based emulsions and only if electrostatic potential was applied. It  
385 has been reported that extrusion of high viscosity polymer solutions (i.e. high concentration  
386 polymer solutions) gives deformed particles having shape of eggs or drops (Prüsse et al., 2008;  
387 Levic et al., 2013). This is again the direct outcome of the polymer flow behaviour in the  
388 electrostatic field: as a result of applied voltage, the spherical shape of the liquid meniscus at the  
389 tip of the needle is deformed into a conical shape. Consequently, the alginate solution flows  
390 through this weak area at an increasing rate, causing formation of a neck and the neck formation  
391 is more pronounced as the alginate solution is more viscous (i.e. more concentrated). After its  
392 detachment and disintegration, the falling linking filaments will solidify into elongated beads

393 (Poncelet, Babak, Neufeld, Goosen, & Bugarski, 1999). After drying process, the sphericity of  
394 the beads was changed toward irregular shapes, which is noticed by values for Sphericity factor  
395 (SF) higher than 0.05, and the worst values are those found for empty beads. The last assertion,  
396 together with the results for the effect of D-limonene on size of dried beads, leads to a conclusion  
397 that the flavour stabilizes beads morphology during drying proces.

398

### 399 **Table 3**

400

401 Additionally, the influence of drying process and the addition of flavour on morphology of beads  
402 was evaluated by SEM (Fig. 6).

403

### 404 **Fig. 6.**

405

406 The images presented in Fig. 6 reveal that the problem of the gel cracking upon drying which  
407 is noticed in case of empty beads (Fig. 6a) is overcome by addition of flavour (Fig. 6c), which,  
408 obviously, acted as a filler. As it can be seen, surface roughness of the 0.02 g/mL Ca-alginate  
409 beads containing 5 % w/w of the flavor (Fig. 6d) was more pronounced compared to the 0.02  
410 g/mL Ca-alginate beads without flavor (Fig. 6b).

411 The shrinkage of beads upon drying is quantified via Shrinkage factor, the values are  
412 presented in Table 3. It seems that the shrinkage factor correlates with the amount the flavor  
413 compound so that the beads shrunk less if they had higher content of the flavour, as there was a  
414 less of water to evaporate. According to the results presented in Table 3, D-limonene was  
415 immobilized within Ca-alginate matrix with efficiency of 50 to ~77%. The values are lower in

416 comparison with the literature data on encapsulation of oily compounds in beads of calcium  
417 alginate by extrusion-dripping technique (Peniche, Howland, Corriño, Zaldívar, & Argüelles-  
418 Monal, 2004; Chang & Dobashi, 2003; Chan, 2011a), but in a good agreement with reports on  
419 encapsulation of some plant aqueous extract (Stojanovic et al., 2012). One of the reasons is that  
420 alginate used in this study is poor in guluronic acid (G) residues (M/G= 1.56), having lower  
421 gelling density at the emulsion droplet surface, thus yielding a lower encapsulation efficiency in  
422 comparison to high G alginates. The immobilization efficiency found for both alginate  
423 concentrations showed the same trend, increasing with the increase in the flavor loading.

424

### 425 *3.3. The rehydration study*

426

427 The rehydration of the dried beads was performed in (1) water and (2) phosphate buffer  
428 (PBS). The results of rehydration tests indicate that swelling of beads depended on the flavor  
429 contents, bead size and alginate concentration. Generally, swelling depends on sub processes  
430 such as: (1) transport of water and  $\text{Na}^+$  ions to gel bead by diffusion mechanism and (2) gel  
431 disintegration caused by partial  $\text{Na}^+$ - $\text{Ca}^{2+}$  ion exchange in case of PBS induced hydration.  
432 Actually, when calcium alginate beads are brought in contact with aqueous medium of higher  
433 pH, ion exchange takes place between the gel-forming  $\text{Ca}^{2+}$  ions and  $\text{Na}^+$  ions of the dissolution  
434 medium. As the  $\text{Ca}^{2+}$  ions are exchanged, electrostatic repulsion between the ionized carboxylate  
435 anions of alginic acid accelerates the swelling and erosion of alginate gel (Kikuchi, Kawabuchi,  
436 Sugihara, Sakurai, & Okano, 1997). Moreover, upon ionization, the counter-ion concentration  
437 inside the polymeric network increases, and an osmotic pressure difference exists between the  
438 internal and external solutions of the beads (Soppimath, Kulkarni, & Aminabhavi, 2001).

439 In water, swelling of the dry beads is mainly attributed to the hydration of the hydrophilic  
440 groups of alginate. Based on experimental results of this study, duration of reversible swelling  
441 ( $t_w$ ) in water was ~20 min. It represented the time needed for elastic volumetric deformation of  
442 gel caused by water input. After this time swelling of Ca-alginate gel in water was equilibrated  
443 as it was shown in Fig. 7a-b. Our results suggest that reversible swelling was more evident for  
444 the smaller (produced by applying voltage) than for the larger beads (produced by simple  
445 dripping technique) and it should be related to larger interface, in the case of the smaller beads.  
446 Reversible swelling was more intensive for 0.03 g/mL Ca-alginate compared to 0.02 g/mL Ca-  
447 alginate beads. This is in accordance with the fact that higher concentration of hydrophilic  
448 alginate chains per bead induced higher water adsorption. Embedding of the flavor within the  
449 beads caused decrease of reversible swelling. It seems that immobilized flavor acted as a  
450 physical barrier for water transport through the gel on one side, and it also suggests that there is  
451 no affinity between alginate and flavour via electrostatic attraction that would otherwise hinder  
452 side-by-side aggregation of alginate egg-box junctions (Vreeker, Li, Fang, Appelqvist, &  
453 Mendes, 2008). Addition of 5 % w/w flavor to 0.02 g/mL Ca-alginate beads didn't have  
454 significant influence on swelling process. However, addition of 10 % w/w flavour to 0.02 g/mL  
455 in case of the smaller beads induced dispersion of experimental data (Fig. 7a-b). The results  
456 indicate a destabilization of 0.02 g/mL alginate gel containing such high amount of the flavor  
457 which occurred during water input. The phenomenon was not observable for the larger beads.

458  
459 **Fig. 7a-b.**

460  
461 Swelling of Ca-alginate gel in phosphate buffer consisted of two contributions: (1) reversible  
462 swelling caused by diffusion of solution into the gel matrix and (2) irreversible swelling caused

463 by partial disintegration of junction zones induced by  $\text{Na}^+$ - $\text{Ca}^{2+}$  ion exchange. In the following  
 464 text, the kinetic equation for estimating the irreversible swelling of empty Ca-alginate gel beads  
 465 will be developed, followed by model modifications for describing the influence of the flavour  
 466 on irreversible swelling.

467 The stability of Ca-alginate can be explained by disintegration of junction zones of the gel  
 468 (Pajić-Lijaković, Plavšić, Bugarski, & Nedović, 2007). Partial  $\text{Na}^+$ - $\text{Ca}^{2+}$  ions exchange and  
 469 corresponding disintegration of the junction zones occurred in the time interval  $t \in (0, t_\infty)$  (where  
 470  $t_\infty \approx 240$  min was the time up to which the beads kept their structural integrity). Density of  
 471 disintegrated junction zones within the Ca-alginate gel was expressed as:  $y(t) \sim M(t)$ , where  $y(t)$   
 472 was the density of disintegrated junction zones and  $M(t)$  was the mass of the solution per mass of  
 473 dry gel which was related to irreversible swelling.

474 In this study, the first order kinetic model equation was used for estimating the disintegration  
 475 of Ca-alginate beads without the flavor in phosphate buffer. The similar modeling equation has  
 476 been already applied for describing swelling of various gel types (Pasparakis & Bouropoulos,  
 477 2006; Ganji, Vasheghani-Farahani, & Vasheghani-Farahani, 2010). The model equation was  
 478 expressed as:

$$479 \quad \frac{dM(t)}{dt} = k(M_\infty - M(t)) \quad (7)$$

480 where  $k$  was the kinetic constant of gel disintegration and  $M_\infty$  was the mass of the solution at  
 481 equilibrium per mass of dry gel which induces irreversible swelling i.e.  $M_\infty = M(t_\infty)$ . The initial  
 482 condition was: at  $t=0$  the corresponding mass was  $M(t=0)=0$ . After solving the model  
 483 Equation (7) was expressed as:

485

$$M(t) = M_{\infty} [1 - e^{-k t}] \quad (8)$$

However, the model Equation (7) should be additionally modified for describing the irreversible swelling of Ca-alginate gel which contains the immobilized flavour. The modification should include the dumping effects caused by the immobilized flavour on the kinetic of gel disintegration. Consequently, fractional derivatives were introduced into Equation (7) for modeling the dumping effects as:

$${}_0^C D_t^{\beta} M(t) = k(M_{\infty} - M(t)) \quad (9)$$

where  ${}_0^C D_t^{\beta}$  was Caputo's fractional derivative operator and the model parameter  $\beta$  represented the dumping coefficient in the range  $0 \leq \beta < 1$ . Lower value of the dumping coefficient indicated higher dumping effects (Podlubny, 1999). We used Caputo's definition of the fractional derivative of the function  $M(t)$ , given as follows (Podlubny, 1999): for  $0 \leq \beta < 1$  the

derivative is  ${}_0^C D_t^{\beta} (M(t)) = \frac{1}{\Gamma(\beta - 1)} \int_0^{t^*} \frac{M(t')^{(1)}}{(t - t')^{\beta}} dt'$ , where  $\Gamma(\beta - 1)$  is gamma function. When the

dumping coefficient tends to one i.e.  $\beta \rightarrow 1$ , the fractional derivative becomes  ${}_0^C D_t^{\beta} \rightarrow \frac{d}{dt}$ . For

such condition, dumping effects could be neglected and the model Equation (7) and Equation (9)

became the same. After solving the model Equation (9) the following expression was derived:

$$M(t) = M_{\infty} [1 - E_{\beta,1}(-k t^{\beta})] \quad (10)$$

where  $E_{\beta,1}(-k t^{\beta})$  was Mittag-Leffler function (Podlubny, 1999) equal to

$$E_{\beta,1}(-k t^{\beta}) = \sum_{k=0}^{\infty} \frac{(-k t^{\beta})^k}{\Gamma(1 + \beta k)}$$



509 The model parameters: the kinetic constant  $k$  and the dumping coefficient  $\beta$  were determined  
510 during fitting procedure by comparing experimental data with the model predictions calculated  
511 using Equation (8) for the gel without the flavor and Equation (10) for the gel with the  
512 immobilized flavour.

513 The model predictions and experimental data on Ca-alginate gel swelling, with and without  
514 the immobilized flavour, are shown in Fig. 8a-b.

515  
516 **Fig. 8a-b.**

517  
518 Similarly as in the case of swelling in water, it can be seen in Fig. 8a-b that swelling in  
519 phosphate buffer was more pronounced for the smaller Ca-alginate beads, most probably due to  
520 larger contact surface. Irreversible swelling of 0.02 g/mL Ca-alginate gel was approximately the  
521 same as for 0.03 g/mL Ca-alginate gel for the samples with and those without the flavour. These  
522 data are in accordance with the fact that both types of beads contain approximately the same  
523 concentration of junction zones, owing to the same concentration of  $\text{CaCl}_2$  used in all  
524 experiments. Irreversible swelling seems to be less pronounced as the amount of flavor increases.  
525 It seems that droplets of the flavour have a role of barrier for solute transport; thus making  
526 impossible for  $\text{Na}^+$  ions to fill some parts of gel and to induce disintegration. Consequently, the  
527 presence of flavor induced damping effects of the gel disintegration process. Such complex  
528 phenomenon was estimated based on the developed mathematical model.

529 The values of  $M(t)$ , obtained from the previously explained mathematical model correlate  
530 satisfactory with the experimental data, with a relative error of 10% for the larger beads and 15%  
531 for the smaller beads. The optimal model parameters that enabled the best comparison between  
532 the experimental and calculated data are shown in Table 4.

533  
534  
535

**Table 4**

536 The kinetic constant for gel disintegration  $k$  was found to be dependent on the interface area.  
537 Consequently, 1.42 times higher value of  $k$  is obtained for the smaller beads due to larger  
538 interface. On the other side, the dumping coefficient  $\beta$  is dependent on: (1) the bead size, (2) the  
539 immobilized amount of the flavour within the beads and (3) the concentration of alginate. The  
540 dumping effects were pronounced for larger beads due to lower interface. On the other side,  
541 higher amount of the flavour induced more evident dumping effects which were quantified by  
542 lower values of  $\beta$ . These results indicate that, in the case of higher amount of the immobilized  
543 flavour, bigger parts of gel porous structure were not available to disintegration process caused  
544 by  $\text{Na}^+$  ions diffusion. Dumping effects were slightly higher for 0.03 g/mL Ca-alginate compared  
545 to 0.02 g/mL Ca-alginate beads.

546  
547

548 *3.4. Thermal stability of D-limonene within the Ca-alginate beads*

549

550 The thermal stability of immobilized D-limonene was studied by using simultaneous  
551 thermogravimetric/mass spectrometry (TG/MS) analysis. The results of thermal analysis are  
552 shown in Fig. 9.

553

554 **Fig. 9.**

555

556 Simultaneous mass spectrometry analysis of released gaseous products was used to  
557 differentiate the steps in thermal release of the immobilized flavour. Two characteristic mass-to-

558 charge ratios ( $m/z$ ) were monitored: ( $m/z$ ) = 17 for water release detection and ( $m/z$ ) = 68 for D-  
559 limonene detection. These  $m/z$  values were selected from the mass spectra database as specific  
560 for targeted compounds, as explained previously. In the case of beads with flavour, water release  
561 was observed in the temperature range from 40°C to 180°C, with a peak at around 75°C and a  
562 decreasing signal up to 180°C. According to the literature, it is related to evaporation of different  
563 type of water from the polysaccharides (Laurienzo, Malinconico, Motta, & Vicinanza, 2005).  
564 Our results indicated that the weight loss for empty beads was about 15%. According to Lević et  
565 al. (2011), the majority of free D-limonene evaporated up to 200°C. As it can be seen from Fig.  
566 9, the release of D-limonene occurs in temperature range from 60°C to 200°C. This was verified  
567 by observation of the characteristic  $m/z$  value ( $m/z=68$ ) of D-limonene released during analysis.  
568 The weight loss in the applied temperature range was ~35%. Our results pointed that most of the  
569 immobilized D-limonene remained intact inside Ca-alginate matrix during the applied  
570 temperature regime. This is desirable effect of immobilization, especially because the applied  
571 temperature range of thermal analysis is in accordance with the temperature regime which  
572 corresponds to the conditions for thermally processed food (De Roos, 2003; 2006).

573

#### 574 **4. Conclusion**

575

576 The results of this study showed that Ca-alginate beads are the suitable carriers for  
577 embedding of D-limonene in order to keep its thermal stability. It is also in accordance with the  
578 facts that the beads with up to 10 % w/w of D-limonene keep their structural integrity during: (1)  
579 drying process, (2) reversible swelling in water and (3) irreversible swelling in phosphate buffer.

580 Action of Na<sup>+</sup> ions from phosphate buffer induces only partial disintegration of Ca-alginate  
581 network.

582 However, dispersed D-limonene represents the physical barrier to: (1) water evaporation  
583 during drying, (2) water diffusion during reversible swelling and (3) Na<sup>+</sup> ions diffusion during  
584 irreversible swelling. The partial disintegration of Ca-alginate network is modeled kinetically by  
585 introducing the dumping effects in the form of fractional derivatives.

586 The size and shape of the beads depend on the rheological behavior of Na alginate/D-  
587 limonene emulsions and could be regulated by applying electrostatic field during the  
588 immobilization process. D-limonene influences structural ordering of alginate chains in flow  
589 field and induces increase in viscosity and reduction in conductivity of the liquid systems.

590 Dispersed D-limonene remains thermally stable inside Ca-alginate matrix within the  
591 temperature regime up to 200°C based on TG/MS analysis. It corresponds to the temperature  
592 regime for the bead application in food technology.

593

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597

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**Table 1**

The composition of the liquid systems used for immobilization process.

Formulation no.	Sample	Na-alginate concentration (g/mL)	D-limonene concentration (% w/w)	Applied voltage (kV)
1	$S_{0.02}^0$	0.02	0	0
2	$S_{0.03}^0$	0.03	0	0
3	$S_{0.02}^5$	0.02	5	0
4	$S_{0.03}^5$	0.03	5	0
5	$S_{0.02}^{10}$	0.02	10	0
6	$S_{0.03}^{10}$	0.03	10	0
7	$S_{0.02}^0$	0.02	0	6.5
8	$S_{0.03}^0$	0.03	0	6.5
9	$S_{0.02}^5$	0.02	5	6.5
10	$S_{0.03}^5$	0.03	5	6.5
11	$S_{0.02}^{10}$	0.02	10	6.5
12	$S_{0.03}^{10}$	0.03	10	6.5

**Table 2** The properties of the liquid systems: conductivity, emulsions stability, the average droplet size and power-law model fitting parameters.

Sample	Conductivity (mS/cm)	Emulsion stability (%)	Average droplet size ( $\mu\text{m}$ )	Homogenous subsets of average flavour droplet size*	Parameters of the power-law model		
					$k$ ( $\text{Pa}\cdot\text{s}^n$ )	$n$	$R^2$
$S_{0.02}^0$	3.94 $\pm$ 0.01	-	-	-	1.98 $\pm$ 0.29	0.63 $\pm$ 0.02	0.995
$S_{0.03}^0$	5.72 $\pm$ 0.07	-	-	-	9.00 $\pm$ 1.36	0.54 $\pm$ 0.02	0.993
$S_{0.02}^5$	3.67 $\pm$ 0.11	98.7 $\pm$ 1.2	4.9 $\pm$ 2.2	1	2.32 $\pm$ 0.32	0.62 $\pm$ 0.02	0.995
$S_{0.03}^5$	5.44 $\pm$ 0.30	98.0 $\pm$ 1.6	6.9 $\pm$ 6.3	1,2	9.72 $\pm$ 1.34	0.53 $\pm$ 0.02	0.992
$S_{0.02}^{10}$	3.36 $\pm$ 0.21	97.4 $\pm$ 1.9	7.5 $\pm$ 5.0	2	2.76 $\pm$ 0.42	0.60 $\pm$ 0.02	0.993
$S_{0.03}^{10}$	4.95 $\pm$ 0.43	97.5 $\pm$ 2.3	11.7 $\pm$ 11.0	3	11.80 $\pm$ 1.17	0.50 $\pm$ 0.01	0.987

\* Homogeneous subsets of flavour droplet means for different solutions, obtained from Tukey's test.

**Table 3** The morphological characteristics and immobilization efficiency of beads produced with and without applying electrostatic force

Formulation no.	Sample	Beads size		Sphericity factor		Shrinkage factor (k <sub>SF</sub> (drying))***	Immobilization efficiency (%)	Homogenous subsets (Tukey test)****
		wet beads	dried beads	wet beads*	dried beads**			
1	S <sub>0.02</sub> <sup>0</sup>	2184±81	846±123	0.008	0.10	0.61	-	4
2	S <sub>0.03</sub> <sup>0</sup>	2215±63	851 ± 97	0.004	0.054	0.61	-	4
3	S <sub>0.02</sub> <sup>5</sup>	2331±92	1078±65	0.023	0.051	0.54	54.5 ± 10.7	4,5
4	S <sub>0.03</sub> <sup>5</sup>	2173±46	1067±56	0.01	0.032	0.51	63.4 ± 4.4	4,5
5	S <sub>0.02</sub> <sup>10</sup>	2288±84	1287±79	0.012	0.019	0.44	70.3 ± 0.7	5
6	S <sub>0.03</sub> <sup>10</sup>	2247±64	1285±99	0.006	0.067	0.43	68.3 ± 5.6	5
7	S <sub>0.02</sub> <sup>0</sup>	975± 43	331±42	0.01	0.07	0.66	-	1
8	S <sub>0.03</sub> <sup>0</sup>	1143±91	432±98	0.003	0.188	0.62	-	1,2,3
9	S <sub>0.02</sub> <sup>5</sup>	968 ± 51	442±38	0.016	0.048	0.54	60.6 ± 5.5	1
10	S <sub>0.03</sub> <sup>5</sup>	1334±248	649±139	0.16	0.165	0.51	52.7 ± 3.0	2,3
11	S <sub>0.02</sub> <sup>10</sup>	968±47	571±50	0.016	0.055	0.41	77.3 ± 3.7	1,2
12	S <sub>0.03</sub> <sup>10</sup>	1452±352	811±165	0.21	0.183	0.44	67.1 ± 4.8	3

\* the average absolute deviation less than 11%

\*\* the average absolute deviation less than 23%

\*\*\* the average absolute deviation less than 23%

\*\*\*\* Homogeneous subsets of beads means for different solutions, obtained from Tukey's test.

**Table 4**

The model parameters for irreversible swelling of the beads.

Formulation no.	Sample	$k$ ( $\text{min}^{-1}$ )	$\beta$ (-)
1	$S_{0.02}^0$	$(1.2 \pm 0.1) \times 10^{-2}$	1
2	$S_{0.03}^0$	$(1.2 \pm 0.1) \times 10^{-2}$	1
3	$S_{0.02}^5$	$(1.2 \pm 0.1) \times 10^{-2}$	$0.95 \pm 0.01$
4	$S_{0.03}^5$	$(1.2 \pm 0.1) \times 10^{-2}$	$0.94 \pm 0.01$
5	$S_{0.02}^{10}$	$(1.2 \pm 0.1) \times 10^{-2}$	$0.92 \pm 0.01$
6	$S_{0.03}^{10}$	$(1.2 \pm 0.1) \times 10^{-2}$	$0.91 \pm 0.01$
7	$S_{0.02}^0$	$(1.7 \pm 0.1) \times 10^{-2}$	1
8	$S_{0.03}^0$	$(1.7 \pm 0.1) \times 10^{-2}$	1
9	$S_{0.02}^5$	$(1.7 \pm 0.1) \times 10^{-2}$	$0.95 \pm 0.02$
10	$S_{0.03}^5$	$(1.7 \pm 0.1) \times 10^{-2}$	$0.92 \pm 0.02$
11	$S_{0.02}^{10}$	$(1.7 \pm 0.1) \times 10^{-2}$	$0.93 \pm 0.02$
12	$S_{0.03}^{10}$	$(1.7 \pm 0.1) \times 10^{-2}$	$0.90 \pm 0.02$

1 **Figure Captions**

2

3 **Fig. 1.** Electrostatic immobilization process: (a) schematic of the set-up; b) photographs of  
4 emulsion flow and droplets formation under no voltage (b1) and under applied voltage of 6.5 kV  
5 (b2).

6 **Fig. 2.** Viscosity as function of shear rate for the liquid systems. Closed and open symbols  
7 represent up-curve and down-curve, respectively (as also indicated by up-arrow and down-arrow,  
8 respectively).

9 **Fig. 3.** Size distribution of D-limonene droplets in four different liquid systems of Na-alginate-  
10 D-limonene:  $S_{0.02}^5$ ,  $S_{0.02}^{10}$ ,  $S_{0.03}^5$  and  $S_{0.03}^{10}$ .

11 **Fig. 4.** Box-plots of wet (a) and dried (b) beads diameters. The systems formulations and  
12 preparation conditions are listed in Table 1 (see above).

13

14 **Fig.5. A.** Beads produced without applying electrostatic force:  $S_{0.02}^0$  (1-wet, 2-dry);  $S_{0.03}^0$  (3-wet,  
15 4-dry),  $S_{0.02}^5$  (5-wet, 6-dry),  $S_{0.03}^5$  (7-wet, 8-dry),  $S_{0.02}^{10}$  (9-wet, 10-dry),  $S_{0.03}^{10}$  (11-wet, 12-dry).

16 B. Beads produced by applying electrostatic force (6.5kV): (1-wet, 2-dry); (3-wet, 4-dry),  
17 (5-wet, 6-dry), (7-wet, 8-dry), (9-wet, 10-dry), (11-wet, 12-dry).

18

19 **Fig. 6.** SEM images of the 0.02 g/mL Ca-alginate beads - a) without the flavour, low  
20 magnification; b) without the flavour, high magnification, c) with 5 % w/w of the flavour, low  
21 magnification, d) with 5 % w/w of the flavour, high magnification.

22

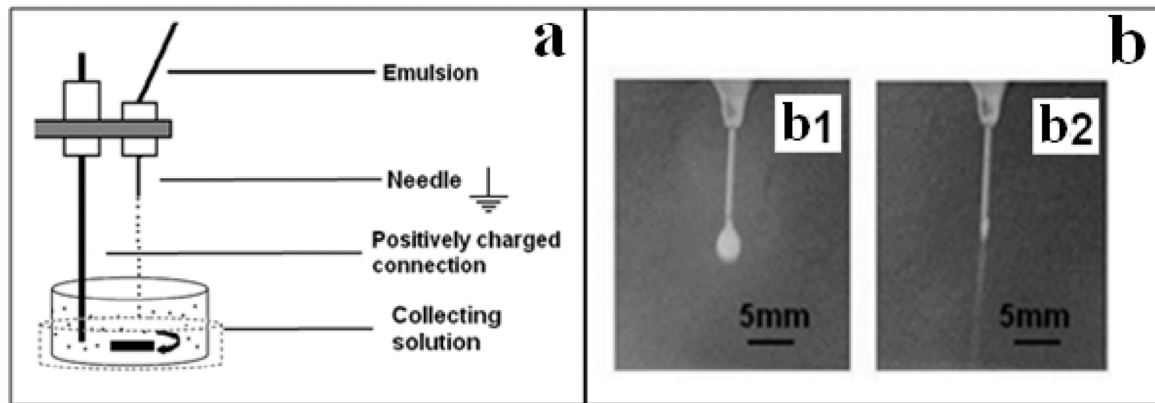
23 **Fig. 7a-b.** a) Swelling kinetics in water: larger beads of 0.02 g/mL Ca-alginate ( $\times$ -empty beads;  
24  $\Delta$ -beads with 5% w/w flavour;  $\square$ -beads with 10% w/w flavour) and 0.03 g/mL Ca-alginate ( $\circ$ -  
25 empty beads;  $*$ -beads with 5% w/w flavour;  $\star$ -beads with 10% w/w flavour). b) Reversible  
26 swelling of smaller beads of 0.02 g/mL Ca-alginate ( $\times$ -empty beads;  $\Delta$ -beads with 5% w/w  
27 flavour;  $\square$ -beads with 10% w/w flavour) and 0.03 g/mL Ca-alginate ( $\circ$ -empty beads;  $*$ -beads  
28 with 5% w/w flavour;  $\star$ -beads with 10% w/w flavour).

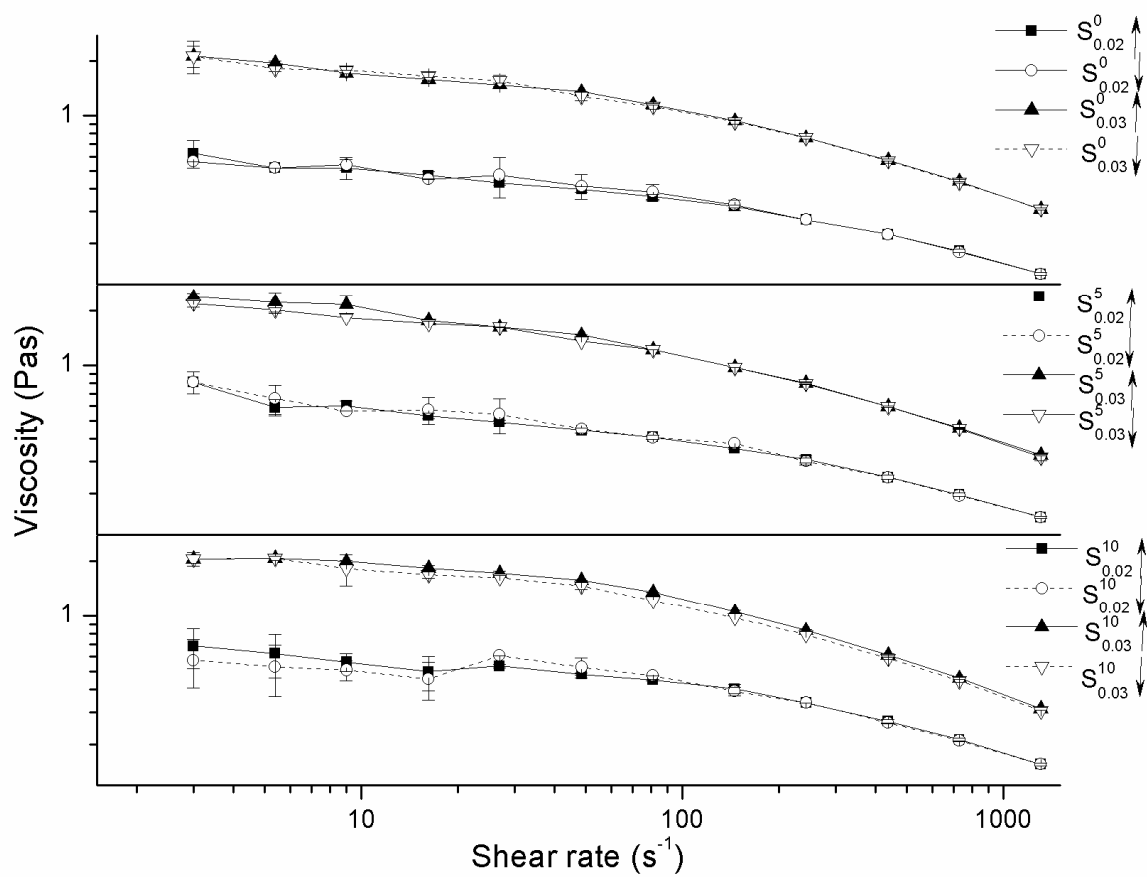
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30 **Fig. 8a-b.** Swelling kinetics in PBS: a) Irreversible swelling of larger beads of 0.02 g/mL with  
31 model predictions (given as lines):  $\square$ -empty beads (solid line),  $\circ$ -beads with 5w/w flavor (dot  
32 line),  $\Delta$ -beads with 10%w/w flavour (short-long dashed line with points). Beads of 0.03 g/mL  
33 Ca-alginate:  $\blacksquare$ - empty beads (dashed line),  $\bullet$ -beads with 5%w/w flavor (dot dashed line),  $\blacktriangle$ -  
34 beads with 10%w/w flavor (short dashed line with points). b) Irreversible swelling of smaller  
35 beads of 0.02 g/mL with model predictions (given as lines):  $\square$ -empty beads (solid line),  $\circ$ -beads  
36 with 5w/w flavour(dot line),  $\Delta$ -beads with 10% w/w flavour (short-long dashed line with points).  
37 Beads of 0.03 g/mL Ca-alginate:  $\blacksquare$ - empty beads (dashed line),  $\bullet$ -beads with 5%w/w flavour  
38 (dot dashed line),  $\blacktriangle$ - beads with 10%w/w flavour (short dashed line with points).

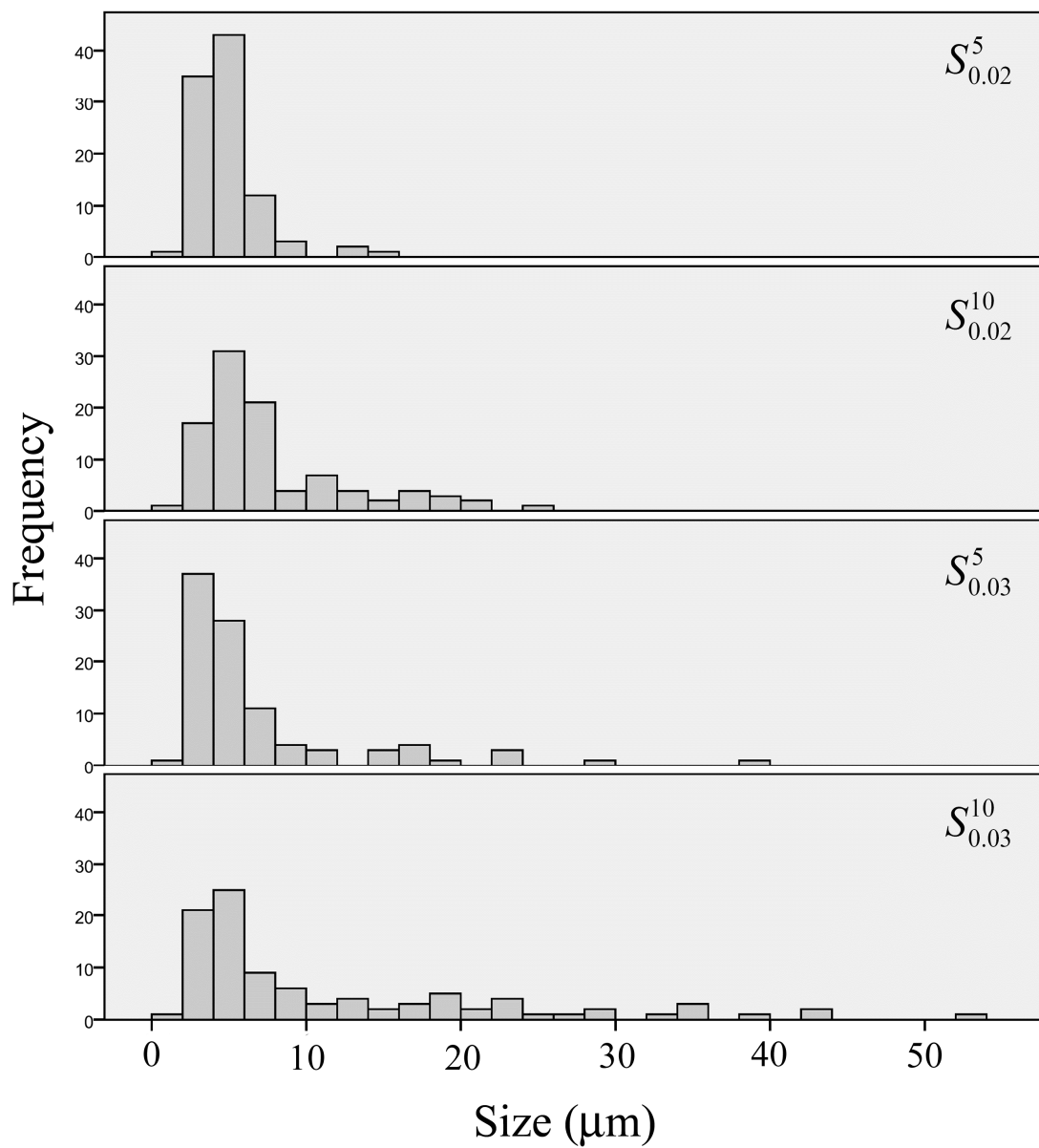
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40 **Fig. 9.** TG/MS profiles obtained for immobilized D-limonene in dried Ca-alginate beads  
41 (Formulation  $S_{0.02}^{10}$ )-TG ( $\square$ ); MS signal (ion current intensity, A) - (m/z)=68 (gray line), (m/z)=17  
42 (black line). TG ( $\Delta$ ) of blank dried alginate beads (Formulation  $S_{0.02}^0$ ).

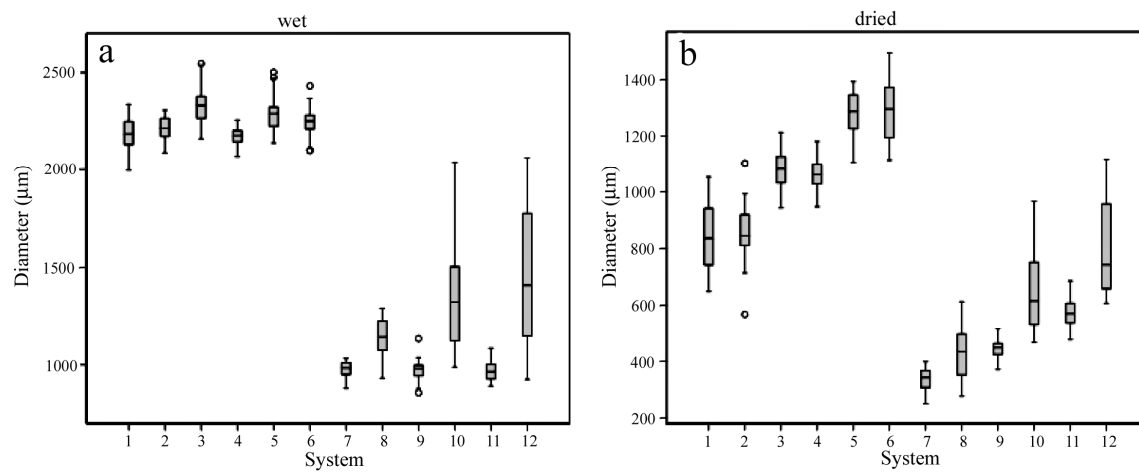
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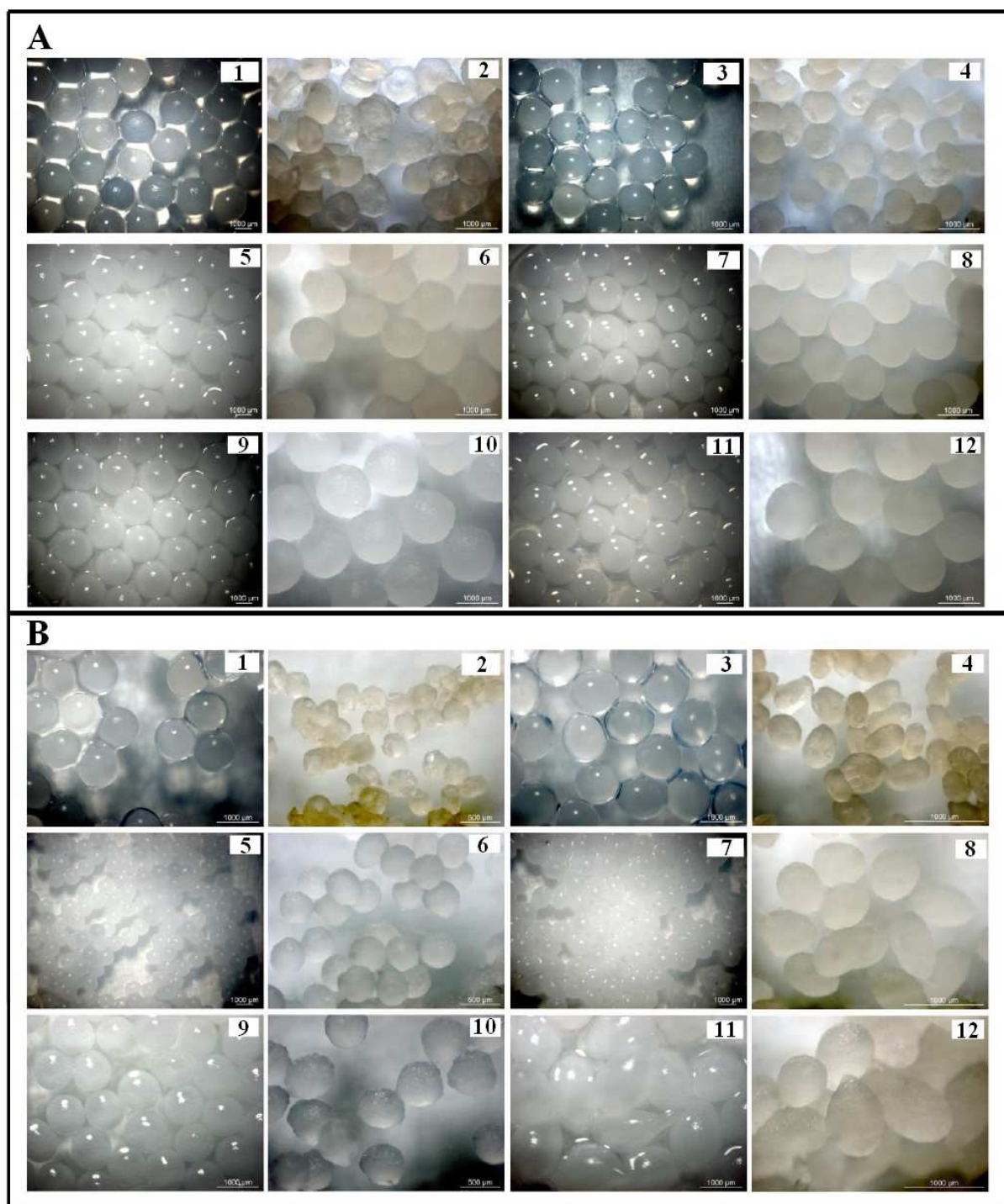


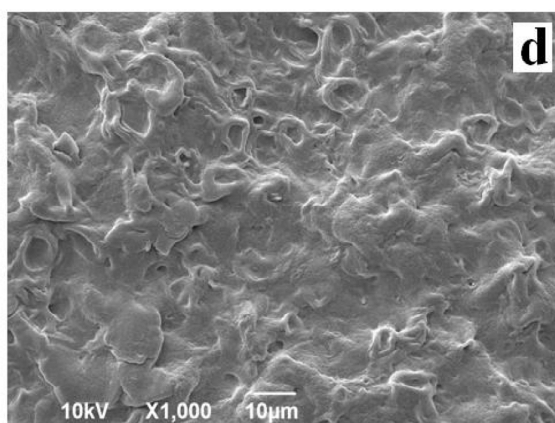
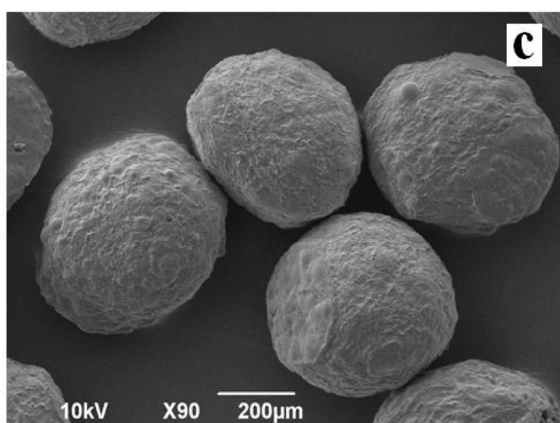
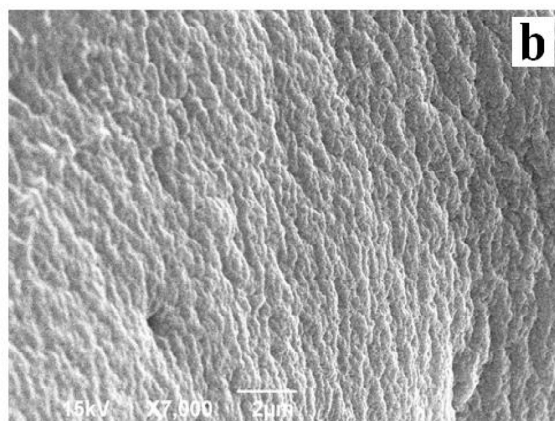
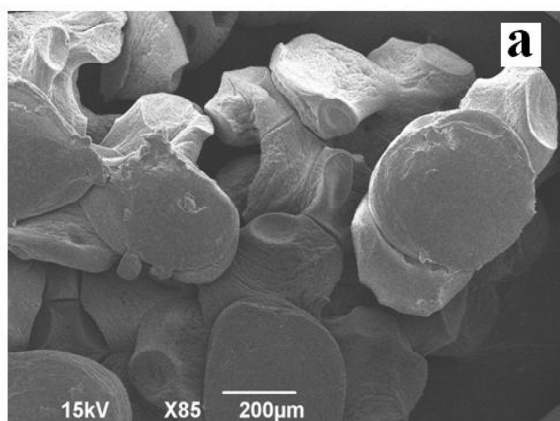




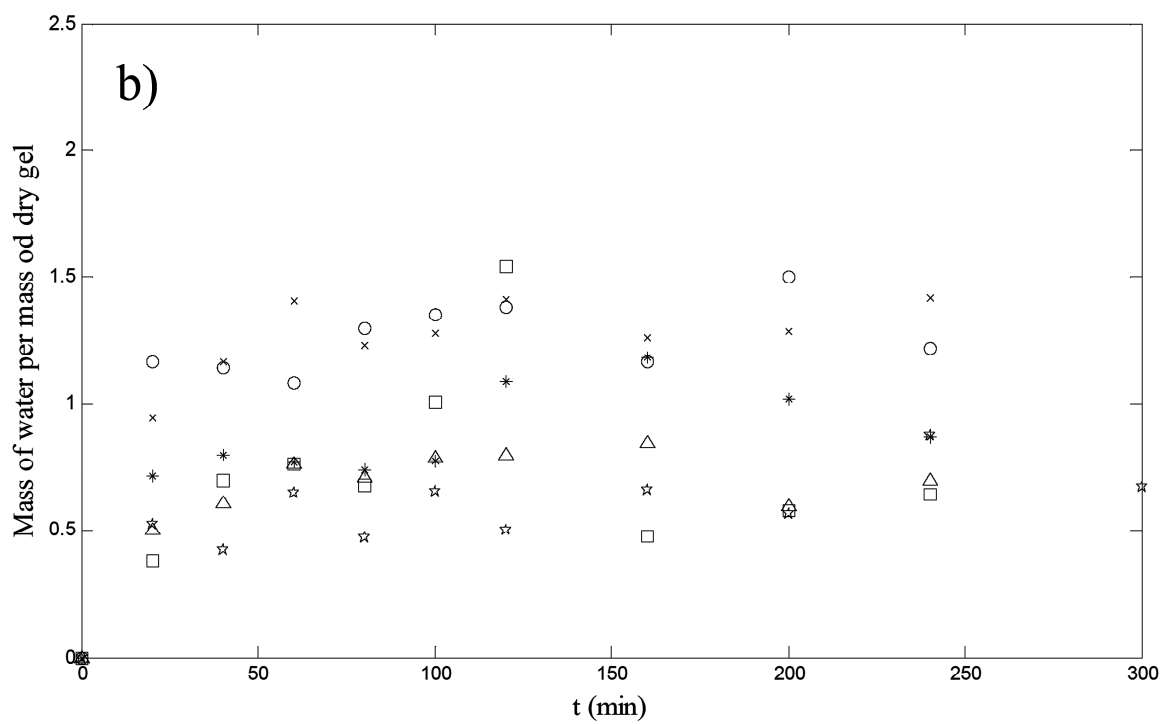
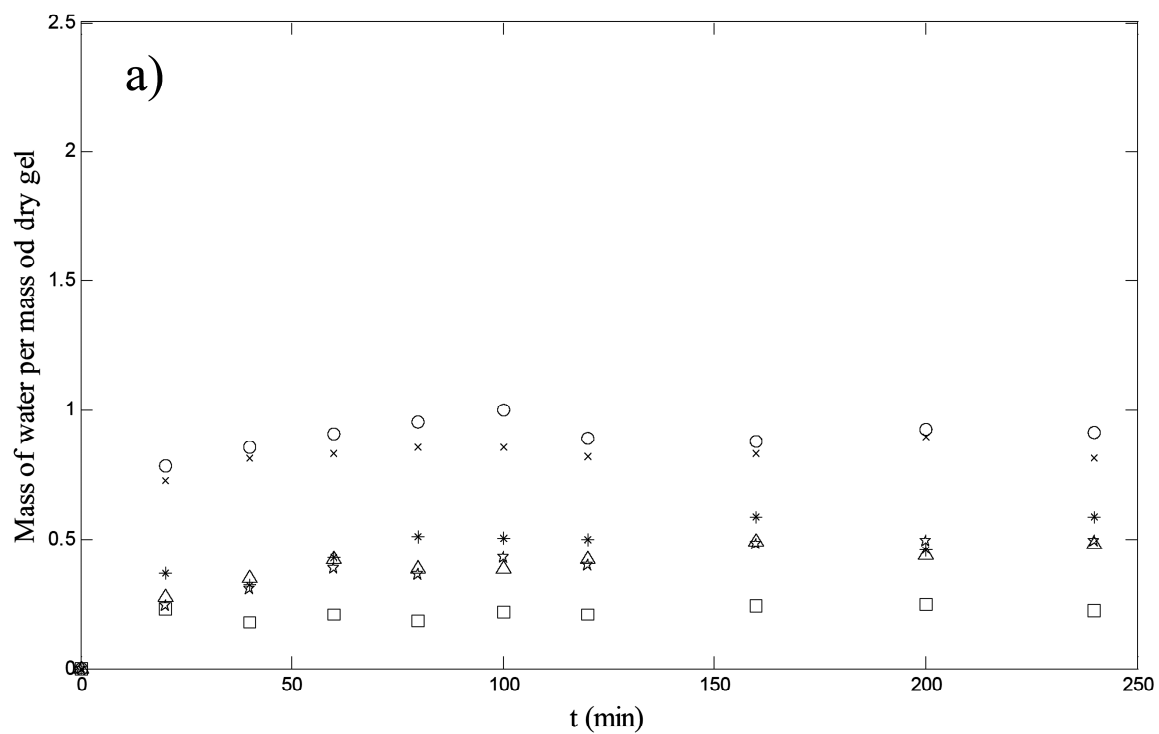


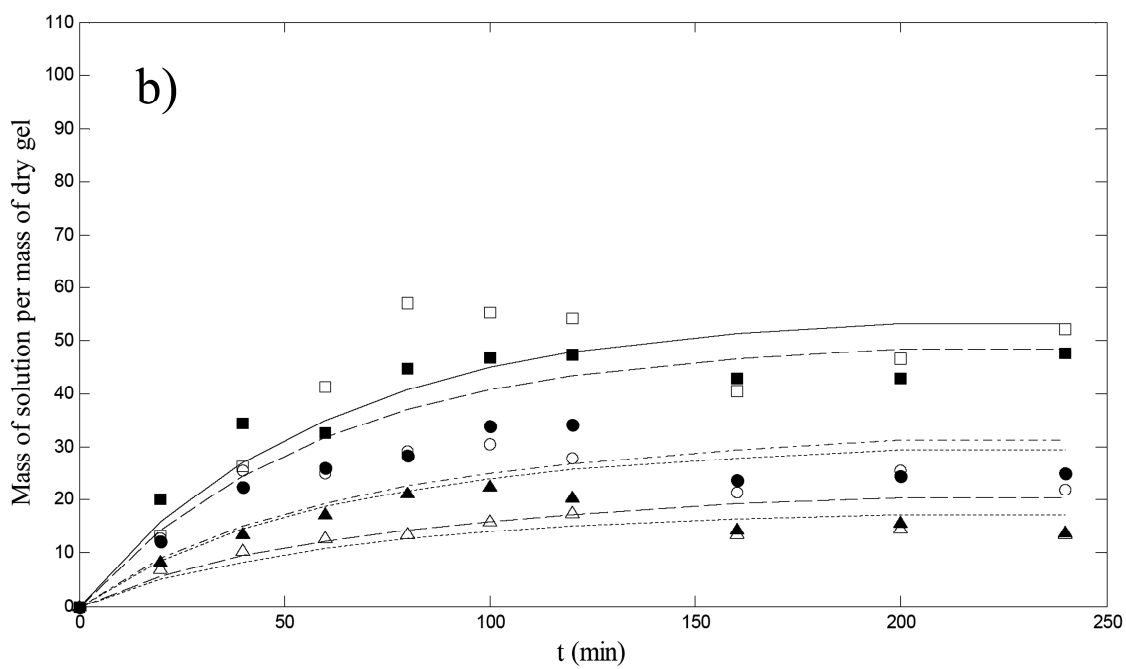
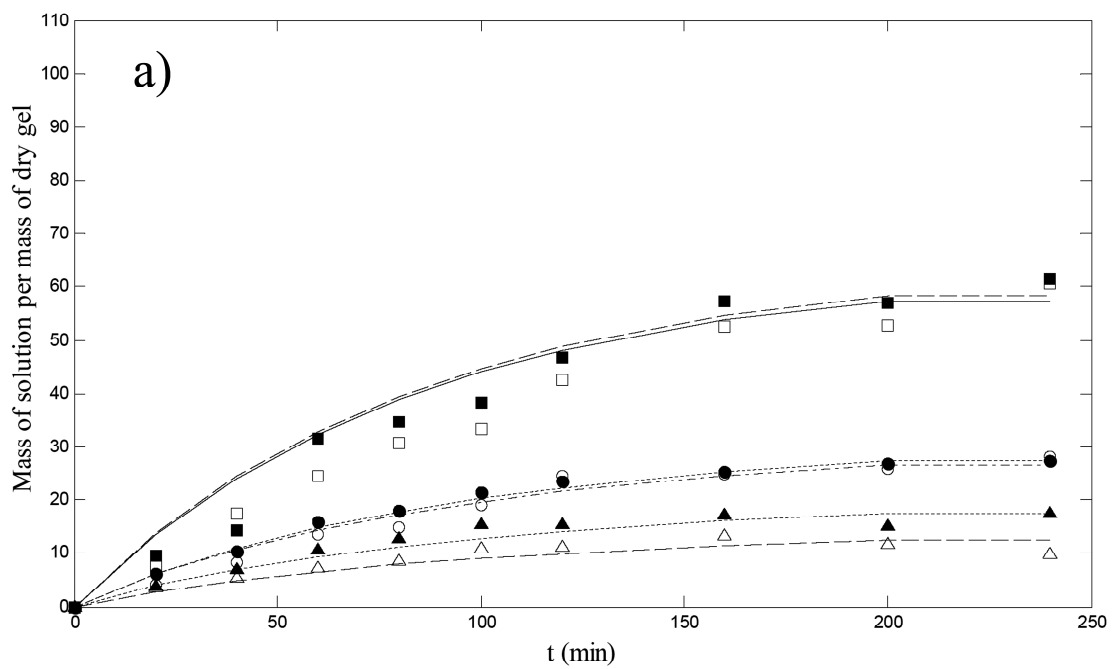




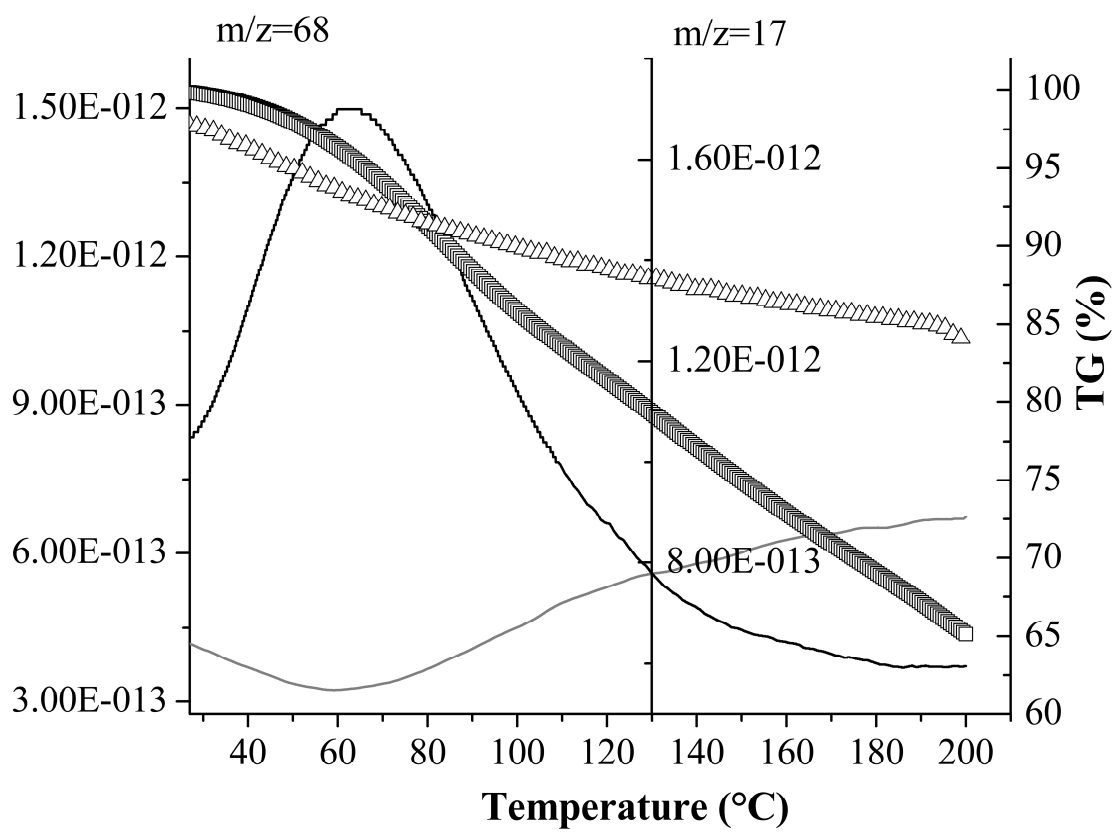


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**Highlights**

- Alginate is used as carrier for D-limonene immobilization.
- Beads loading D-limonene are produced by using electrostatic extrusion.
- D-limonene is immobilized within Ca-alginate matrix with efficiency of 50 to ~77%.
- The dried beads are rehydrated and mathematical model of rehydration is developed.
- Immobilization significantly affects thermal properties of D-limonene.